

# STRENGTH CHARACTERISTICS OF PS ASH-TREATED SAND FOR APPLICATION AS BACKFILL SAND AROUND UNDERGROUND PIPES AND MANHOLES

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## 1. INTRODUCTION

So far, cement or lime has been often added to increase the strength of backfill sand. However, the treated sands sometimes induce high alkalinity or excessive solidification after a long curing period which can be a concern in the re-excavation ability. To solve these issues, this paper attempted to evaluate the short- and long-term strength development of PSAS-treated sand by conducting unconfined compression test and interpreting its strength mechanism using XRD diffraction profiles.

## 2. MATERIALS AND EXPERIMENT PROCEDURE

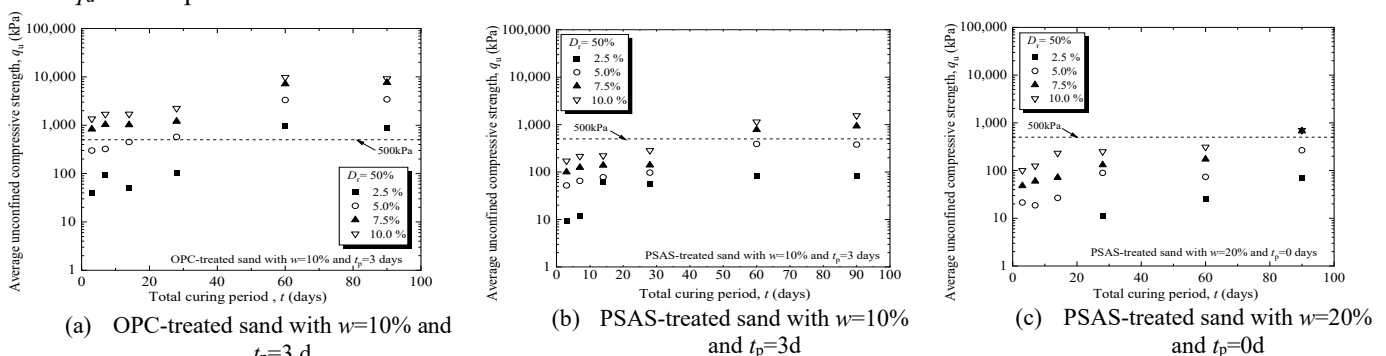
Toyoura sand and a PS ash-based stabilizers (hereafter PSAS) were used. The PSAS-treated sand specimens were prepared with and without primary curing. To prepare the specimens with primary curing, PSAS was mixed with Toyoura sand at addition ratio of PSAS,  $A_{PS}$ , of 2.5%, 5.0%, 7.5%, and 10.0%, and the water content  $w$  was adjusted to 10%. The mixtures were then placed into cylindrical plastic molds (50 mm in diameter and 100 mm in height), compacted to achieve relative density,  $D_r$ , of 50% and 90%, and the molds were sealed for  $t_p = 3$  days for primary curing. Then, the specimens in the molds were cured in water for specified periods  $t_s$  after the primary curing, as shown in Table 1. For comparison, OPC-treated sand specimens with addition ratio of OPC,  $A_{OPC}$ , of 2.5%, 5.0%, 7.5%, and 10.0% were also prepared under the same conditions. For specimens without primary curing, PSAS was mixed with Toyoura sand at  $A_{PS} = 2.5\%$ , 5.0%, 7.5%, and 10.0%, and the  $w$  was adjusted to 20% to prepare the specimens as shown in table 1. Subsequently, the mixtures were placed in molds, compacted to achieve  $D_r = 50\%$  and 90%, and cured in water for specified periods  $t_s$ , as shown in Table 1. Three specimens were prepared for each treatment condition.

**Table 1.** Conditions of treated specimens for UCT

$A_{PS}$ (%)	$A_{OPC}$ (%)	$w$ (%)	$D_r$ (%)	$t_p$ (d)	$t_s$ (d)	$t = t_p + t_s$ (d)
2.5, 5.0, 7.5, 10.0		10	50, 90	3	0, 4, 11, 25, 57, 87	3, 7, 14, 28, 60, 90
		20		0	3, 7, 14, 28, 60, 90	
2.5, 5.0, 7.5, 10.0	10	3		0, 4, 11, 25, 57, 87		

## 3. RESULTS AND DISCUSSION

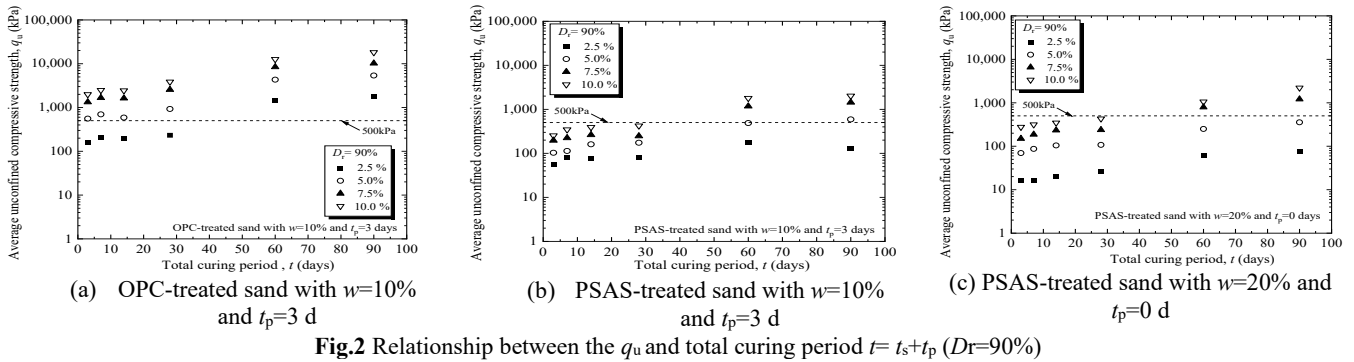
The average unconfined compressive strength  $q_u$  of the three specimens against the total curing days  $t$  for each treatment condition are shown in Figs. 1 and 2. Here, the values of  $q_u$  are plotted on a log scale to make it easier to compare the  $q_u$  of PSAS- and OPC-treated sands. The results for the specimens with  $D_r = 50\%$  and 90% are shown in Figs. 1 and 2, respectively. In each figure, (a) shows the results of OPC-treated sands with  $w = 10\%$  and  $t_p = 3$  d, (b) shows the results of PSAS-treated sands with  $w = 10\%$  and  $t_p = 3$  d, and (c) shows the results of PSAS-treated sands with  $w = 20\%$  and  $t_p = 0$  d. The  $q_u$  of the specimens increased with  $t$  for PSAS- and OPC-treated sands.



**Fig.1** Relationship between the  $q_u$  and total curing period  $t=t_s+t_p$  ( $D_r=50\%$ )

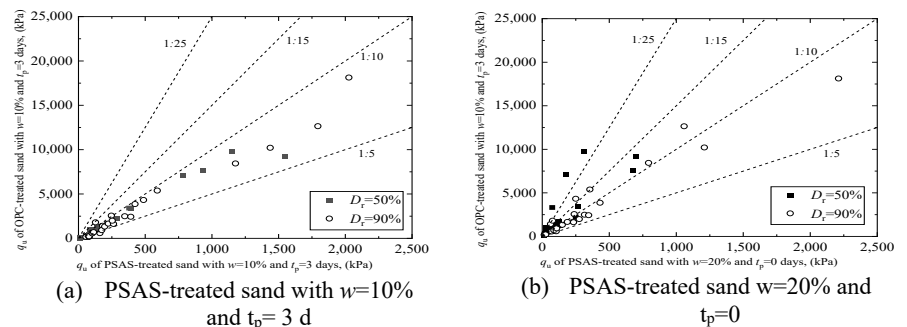
However, the  $q_u$  of the OPC-treated sands was significantly higher than that of the PSAS-treated sands under the same mixing conditions. The  $q_u$  of the OPC-treated sands with  $w = 10\%$  and  $t_p = 3$  d was compared to the  $q_u$  of the PSAS-treated sands with  $w = 10\%$  and  $t_p = 3$  and 0 d, as shown in Fig. 3(a). Similarly, the  $q_u$  of the OPC-treated sands with  $w = 10\%$  and  $t_p = 3$  d was compared to the  $q_u$  of the PSAS-treated sands with  $w = 20\%$  and  $t_p = 0$  d, as shown in Fig. 3(b). The  $q_u$  of the OPC-treated sands were approximately 7.4 to 14.1 times larger than those of the PSAS-treated sands. Hosoya et al. (1993) has demonstrated that a  $q_u$  of 500 kPa or less was desirable for efficient manual excavation without using a pick or breaker. Therefore, the  $q_u$  values of 500 kPa shown as dashed lines in Figs.1 and 2 expressed the maximum value for a backfill sand to be easily re-excavated. The  $q_u$  of OPC-treated sand with  $A_{OPC} = 5\%$  either exceeded 500 kPa from the beginning (Fig.2(a)) or exceeded 500 kPa in the middle of curing (Fig.2(b)). Conversely, the  $q_u$  of PSAS-treated samples with

$A_{PSAS} = 5\%$  barely exceeded 500 kPa during 90 d of curing. This indicates that PSAS-treated sand may be more easily re-excavated than OPC-treated sand.

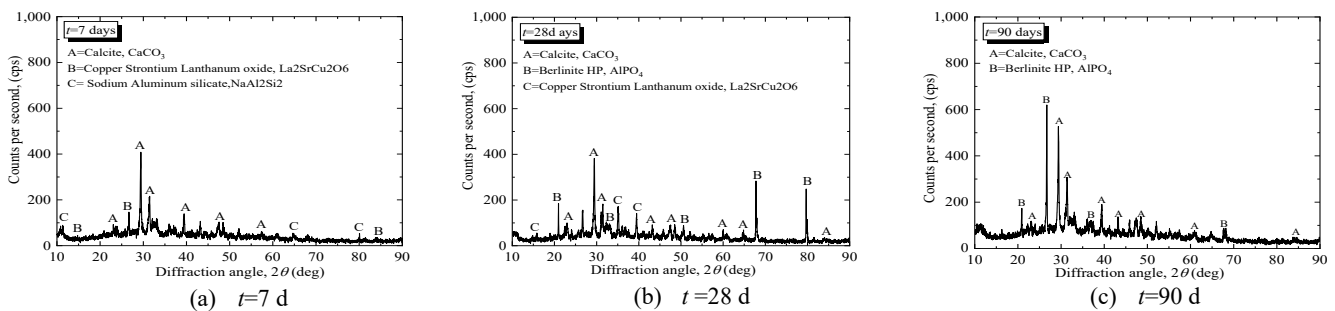


#### 4. XRD PROFILES AND HYDRATES CONTRIBUTING TO THE STRENGTH INCREASE WITH TIME

XRD tests were conducted on PSAS-treated sand that was prepared by mixing PSAS with Toyoura sand with an  $A_{PS}$  of 10% to investigate the hydrates contributing to the strength increase with time. The water content of the mixture was adjusted to 20%. Consequently, the mixtures were placed in molds, compacted to achieve  $D_r = 90\%$ , and cured in water for 7, 28, and 90 days. The XRD results are shown in Fig.4. The XRD pattern revealed that the formation of calcite ( $\text{CaCO}_3$ ) was dominant in the PSAS-treated sand at curing periods of 7, 28, or 90 days. In addition, berlinite ( $\text{AlPO}_4$ ) may be an additional contributor to the increase in the strength of PSAS-treated sand in the long term. The observation of berlinite was similar to that of soils treated with coal ash, as reported by (Zhou et al., 2019).



The XRD results are shown in Fig.4. The XRD pattern revealed that the formation of calcite ( $\text{CaCO}_3$ ) was dominant in the PSAS-treated sand at curing periods of 7, 28, or 90 days. In addition, berlinite ( $\text{AlPO}_4$ ) may be an additional contributor to the increase in the strength of PSAS-treated sand in the long term. The observation of berlinite was similar to that of soils treated with coal ash, as reported by (Zhou et al., 2019).



#### 5. CONCLUSIONS

The unconfined compressive strength  $q_u$  of the PSAS-treated sands increased with the total curing period  $t$ . However, the  $q_u$  of the PSAS-treated sands was significantly lower than that of the OPC-treated sands under the same mixing conditions. The  $q_u$  of the OPC-treated sands was approximately 7.4 to 14.1 times higher than that of the PSAS-treated sands. These observations suggest that PSAS-treated sand is easier to re-excavate than OPC-treated sand. The XRD pattern showed that the formation of calcite ( $\text{CaCO}_3$ ) and berlinite ( $\text{AlPO}_4$ ) was dominant in the PSAS-treated sand in the long term.

#### REFERENCES

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