

## Measurement of Local Strains of Toyoura Sand using Hollow Cylindrical Specimen

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### I) Introduction

During triaxial compression tests on a hollow cylindrical specimen (outer diameter of 20cm, inner diameter of 16cm, and height of 30cm) of Toyoura sand, a sudden reduction was observed in the values of drained quasi-elastic vertical Young's modulus  $E_{eq}$  and shear modulus  $G_{eq}$  that were externally measured by gap sensors at the top cap of the specimen (Koseki et al., 2001). In order to study such peculiar behaviour, a new local measuring device named triangular pin-typed local deformation transducers (triangular P-LDTs) was developed (Hong Nam et al., 2001) to measure four strain components of the hollow cylindrical specimen. Test results on Toyoura sand by using this device are reported herein.

### II) Test Material and Procedures

Dry Toyoura sand (batch G) specimen at an initial void ratio of 0.700 under confining pressure of 30 kPa was prepared by air-pluviation. Figure 1 shows the layout of the transducers, where strain components  $\varepsilon_z$ ,  $\varepsilon_r$ ,  $\varepsilon_\theta$  and  $\gamma_{z\theta}$  were measured locally with two sets of outer triangular P-LDTs and an inner horizontal LDT. In addition, four gap sensors (GS4 through GS7) with a capacity of 4mm were employed to measure the local change in the outer and inner radii. After isotropic consolidation (denoted as IC) up to confining pressure of 450 kPa, the specimen was subjected to drained large cyclic vertical loading (denoted as TC) up to effective vertical stress  $\sigma'_z$  of 400 kPa under constant effective horizontal stresses of  $\sigma'_h (= \sigma'_r = \sigma'_\theta) = 200$  kPa, without/with applying sustained shear stress  $\tau_{z\theta}$  of 50 kPa. At several stress states, the specimen was left for about 10 minutes to achieve stable state, and three small unload/reload cycles were applied in the vertical and torsional directions with a single strain amplitude of 0.001% and 0.0015%, respectively, to evaluate  $E_{eq}$  and  $G_{eq}$ . Measurement of  $\sigma'_z$  and  $\tau_{z\theta}$  was made with a two-component loadcell set inside the triaxial cell.

### III) Results and discussions

Figures 2 and 3 show the locally measured  $E_{eq}$  and  $G_{eq}$  values plotted versus  $\sigma'_z$  and  $(\sigma'_z \cdot \sigma'_h)^{0.5}$ , respectively. In Fig.2, the average of two  $\varepsilon_z$  values that were measured with two sets of triangular P-LDTs was employed. On the other hand, results with a single set of LDTs (Triangular P-LDTs No. 1 in Fig.1) were employed in Fig.3, since the diagonal P-LDT in the other set did not perform properly. It is seen from these figures that  $E_{eq}$  and  $G_{eq}$  can be approximated as linear functions of  $\sigma'_z$  and  $(\sigma'_z \cdot \sigma'_h)^{0.5n}$ , respectively, with  $m=0.45$  and  $n=0.47$ . This  $m$  value is consistent with the one reported by Hoque (1996).

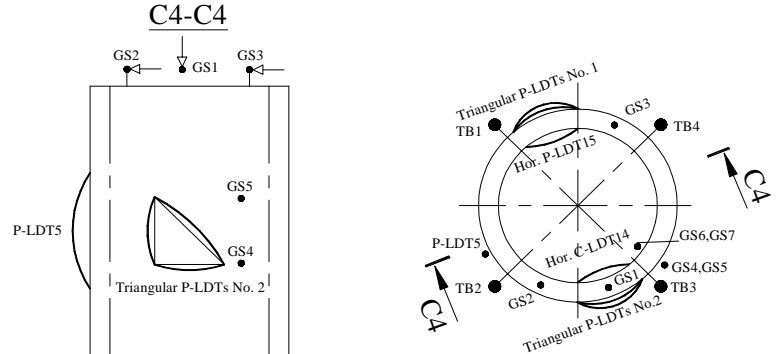


Fig.1 Layout of transducers

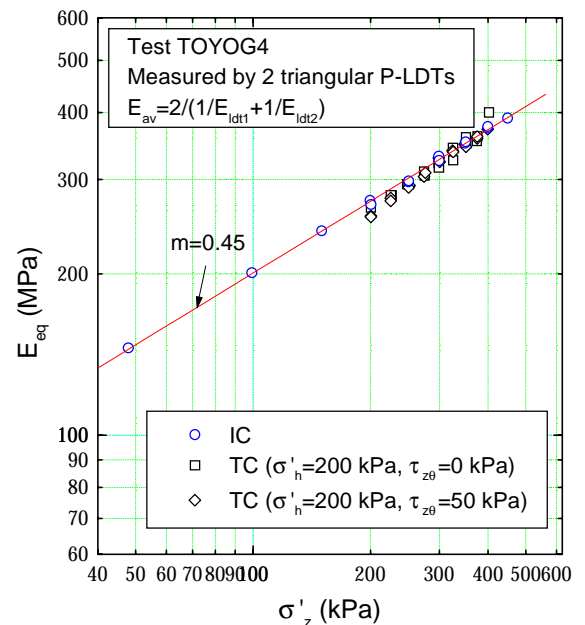


Fig.2  $E_{eq}$  based on average of local strains versus  $\sigma'_z$

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During isotropic consolidation, two  $\varepsilon_z$  values measured with individual set of LDTs were similar. However, during vertical loading with  $\tau_{z\theta}=0$ , sudden distinct changes (decrease on one side and increase on the other side) in these  $\varepsilon_z$  values were observed, which resulted into a disturbance in the relationships between locally evaluated  $E_{eq}$  ( $E_{ldt1}$  and  $E_{ldt2}$  in Fig.4) with individual set of LDTs and  $\sigma'_z$ . In addition, the externally evaluated  $E_{eq}$  values ( $E_{gs}$  in Fig.4) with the vertical gap sensor (GS1 in Fig.1) showed qualitatively a similar response to the ones locally measured on the same side of the specimen (Triangular P-LDTs No.2 in Fig.1), while with a larger extent of disturbance, quantitatively. These behaviours suggest that the specimen was not uniform and/or the loading device was not properly aligned relative to the top surface of the specimen. As a result, after applying a certain level of deviator stress ( $q=100$  kPa in the present test), the distribution of vertical stress and strain increments during small cyclic vertical loading possibly became non-uniform, which affected the external measurement results to a larger extent than the local ones.

As shown in Fig.5, by applying a sustained shear stress of  $\tau_{z\theta}=50$  kPa, the degree of degradation in the externally measured  $E_{eq}$  values was reduced. This may be the result of redistribution of local stresses caused by application of torque.

#### IV) Conclusion

Local measurements of strains in hollow cylindrical specimen of dry Toyoura sand were carried out by using newly developed triangular P-LDTs and gap sensors. Locally measured quasi-elastic  $E_{eq}$  and  $G_{eq}$  values were mainly dependent on the current  $\sigma'_z$  and  $(\sigma'_z \cdot \sigma'_h)^{0.5}$  values, respectively. Non-uniformity of local stresses and strains in the specimen possibly caused a disturbance in the above relationships, to a smaller extent than the external measurements.

#### References

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- 3) Hoque,E., 1996, Elastic deformation of sands in triaxial tests, Doctoral thesis, University of Tokyo.

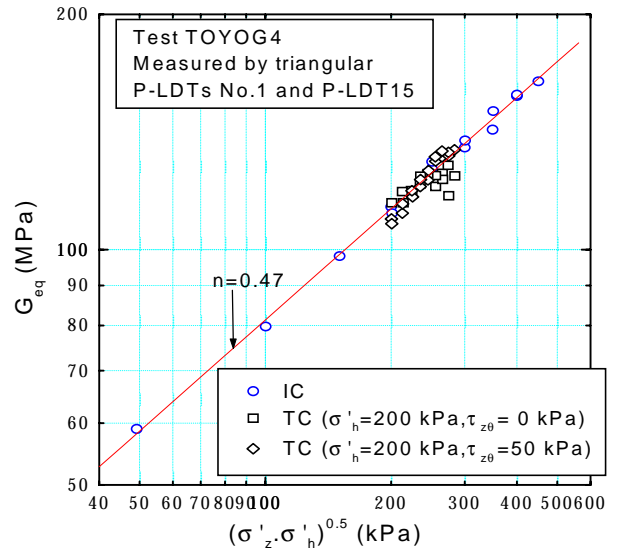


Fig. 3  $G_{eq}$  based on local strain on one side versus  $(\sigma'_z \cdot \sigma'_h)^{0.5}$

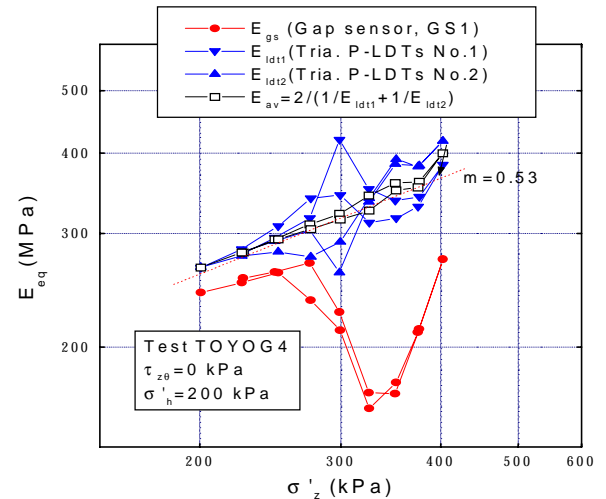


Fig.4 Comparison of  $E_{eq}$  during vertical loading at  $\tau_{z\theta}=0$

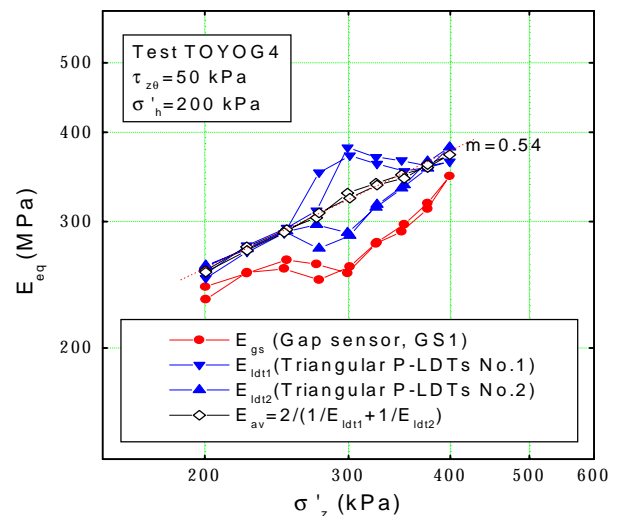


Fig.5 Comparison of  $E_{eq}$  during vertical loading at  $\tau_{z\theta}=50$  kPa