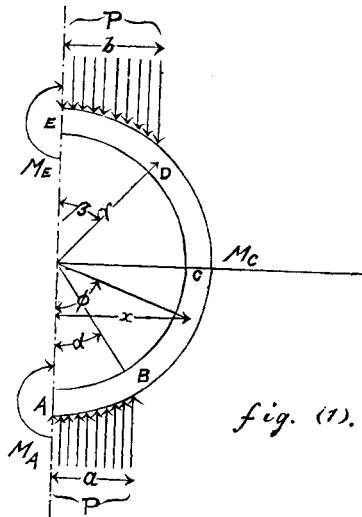


On the calculation of the thin circular pipes under a uniformly distributed load.

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Case I. Bending moment due to external load in thin circular pipe uniformly distributed as shown in the figure (1).

- Let ω = upper load intensity in pound per unit length of horizontal distance.
 ω' = lower load intensity in pound per unit length of horizontal distance.
 C = distance from A measured along the circumference.
 E = modulus of Elasticity of the material.
 I = moment of inertia of the normal section of the pipe.
 A = cross-sectional area of the pipe.



put

$$\omega b = \omega' a = P$$

then

$$\text{and } M_A = X.$$

$$\left\{ \begin{array}{l} \text{Bending moment } (M) \text{ at any point in } AB \\ \qquad \qquad \qquad = X + \frac{\omega' x^2}{2} \\ \text{axial force } (N) \text{ at the same point} \\ \qquad \qquad \qquad = -\omega' x \sin \phi \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

$$\left\{ \begin{array}{l} M \text{ at any point in } BD \\ \qquad \qquad \qquad = X + P\left(x - \frac{a}{2}\right) \\ N \text{ at the same point} \\ \qquad \qquad \qquad = -P \sin \phi \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

$$\left\{ \begin{array}{l} M \text{ at any point in } DE \\ \qquad \qquad \qquad = X + P\left(x - \frac{a}{2}\right) + \frac{\omega(b-x)^2}{2} \\ \qquad \qquad \qquad = X - \frac{Pa}{2} + \frac{Pb}{2} + \frac{\omega x^2}{2} \\ N \text{ at the same point} \\ \qquad \qquad \qquad = -\{P - \omega(b-x)\} \sin \phi = -\omega x \sin \phi. \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

By the principle of least works;

$$\int \frac{M}{EI} \frac{dM}{dX} dx + \int \frac{N}{EA} \frac{dN}{dX} dx = 0$$

Assuming E , I and A constant, we get

$$\int_A^B \left(X + \frac{\omega' x^2}{2} \right) dc + \int_B^D \left(X + Px - \frac{Pa}{2} \right) dc + \int_D^E \left(X - \frac{Pa}{2} + \frac{Pb}{2} + \frac{\omega x^2}{2} \right) dc = 0$$

$$X \int_A^E dc + \frac{\omega'}{2} \int_A^B x^2 dc + P \int_B^D x dc - \frac{Pa}{2} \int_B^E dc + \frac{Pb}{2} \int_D^E dc + \frac{\omega}{2} \int_D^E x^2 dc = 0$$

$$\text{or } X = - \frac{\omega'}{2} \frac{\int_A^B x^2 dc}{\int_A^E dc} - P \frac{\int_B^D x dc}{\int_A^E dc} + \frac{Pa}{2} \frac{\int_B^E dc}{\int_A^E dc} - \frac{Pb}{2} \frac{\int_D^E dc}{\int_A^E dc} - \frac{\omega}{2} \frac{\int_D^E x^2 dc}{\int_A^E dc}$$

Referring to the figure (1), we have

$$x = r \sin \phi$$

$$a = r \sin \alpha$$

$$b = r \sin \beta$$

$$dc = r d\phi$$

ϕ denoting the inclination of the tangent to the horizontal at any point (xy) .

Introducing these values and integrating the terms respectively,

$$\int_A^E dc = r \int_0^\pi d\phi = \pi r$$

$$\int_B^E dc = r \int_\alpha^\pi d\phi = (\pi - \alpha)r$$

$$\int_D^E dc = r \int_{\pi-\beta}^\pi d\phi = \beta r$$

$$\int_B^D x dc = r^2 \int_\alpha^{\pi-\beta} \sin \phi d\phi = r^2 (-\cos \phi)_\alpha^{\pi-\beta}$$

$$\int_A^B x^2 dc = r^3 \int_0^\alpha \sin^2 \phi d\phi = r^3 \left\{ -\frac{\sin 2\phi}{4} + \frac{\phi}{2} \right\}_0^\alpha$$

—(IV)—

$$\int_D^E x^2 dc = r^3 \int_{\pi-\beta}^{\pi} \sin^2 \phi d\phi = r^3 \left\{ -\frac{\sin 2\phi}{4} + \frac{\phi}{2} \right\}_{\pi-\beta}^{\pi}$$

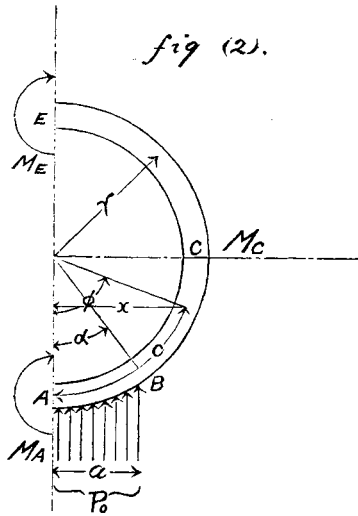
whence we get finally,

$$X(, M_A) = -\frac{Pr}{2\pi \sin a} \left\{ -\frac{\sin 2\phi}{4} + \frac{\phi}{2} \right\}_0^{\alpha} - \frac{Pr}{\pi} (-\cos \phi)_\alpha^{\pi-\beta}$$

$$+ \frac{Pr(\pi-a)\sin a}{2\pi} - \frac{Pr\beta \sin \beta}{2\pi} - \frac{Pr}{2\pi \sin \beta} \left\{ -\frac{\sin 2\phi}{4} + \frac{\phi}{2} \right\}_{\pi-\beta}^{\pi}$$

Case II. Bending moment of thin circular pipe due to its own weight.

(E, I & A all constant)



Let ω = weight in pound per unit length of the circumference.

ω' = Reaction intensity in pound per unit length of horizontal distance.

C = distance from A measured along the circumference.

put $\omega\pi r = \omega'a = P_0$
and $M_A = X$

Then

$$\left\{ \begin{array}{l} \text{Bending Moment } (M) \text{ at any point in } AB \\ = X + \frac{\omega'x^2}{2} - C\omega\left(x - r\sin\frac{\phi}{2}\right) \\ \text{axial force } (N) \text{ at the same point} \\ = -(\omega'x - C\omega)\sin\phi \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

$$\left\{ \begin{array}{l} M \text{ at any point in } BC \\ = X + P_0\left(x - \frac{a}{2}\right) - C\omega\left(x - r\sin\frac{\phi}{2}\right) \\ N \text{ at the same point} \\ = -(P_0 - C\omega)\sin\phi \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

$$\left\{ \begin{array}{l} M \text{ at any point in } CE \\ = X + P_0\left(x - \frac{a}{2}\right) - (\pi r - C)\omega\left\{x - r\sin\frac{\pi - \phi}{2}\right\} \\ + 2\left(C - \frac{\pi r}{2}\right)\omega\left\{r\cos\left(\frac{\phi}{2} - \frac{\pi}{4}\right) - x\right\} \\ = X + P_0x - \frac{P_0a}{2} - C\omega x + P_0r\left(1 - \frac{1}{\sqrt{2}}\right)\cos\frac{\phi}{2} + C\omega r(\sqrt{2} - 1)\cos\frac{\phi}{2} \\ + \sqrt{2}C\omega r\sin\frac{\phi}{2} - \frac{P_0r}{\sqrt{2}}\sin\frac{\phi}{2} \\ N \text{ at the same point} \\ = -(P_0 - C\omega)\sin\phi \\ \therefore \frac{dM}{dX} = 1 \quad \text{and} \quad \frac{dN}{dX} = 0 \end{array} \right.$$

— (VI) —

By putting $\int \frac{M}{EI} \frac{dM}{dX} dc + \int \frac{N}{EA} \frac{dN}{dX} dc = 0$

we obtain

$$\int_A^B \left(X + \frac{\omega' x^2}{2} - C\omega x + C\omega r \sin \frac{\phi}{2} \right) dc + \int_B^C \left(X + P_0 x - \frac{P_0 a}{2} - C\omega x + C\omega r \sin \frac{\phi}{2} \right) dc$$

$$+ \int_C^E \left\{ X + P_0 x - \frac{P_0 a}{2} - C\omega x + P_0 r \left(1 - \frac{1}{\sqrt{2}} \right) \cos \frac{\phi}{2} + C\omega r (\sqrt{2} - 1) \cos \frac{\phi}{2} \right.$$

$$\left. + \sqrt{2} C\omega r \sin \frac{\phi}{2} - \frac{P_0 r}{\sqrt{2}} \sin \frac{\phi}{2} \right\} dc = 0$$

$$X \int_A^E dc + \frac{\omega'}{2} \int_A^B x^2 dc + P_0 \int_B^E x dc - \frac{P_0 a}{2} \int_B^E dc - \omega \int_A^E C x dc$$

$$+ \omega r \int_A^C C \sin \frac{\phi}{2} dc + P_0 r \left(1 - \frac{1}{\sqrt{2}} \right) \int_C^E \cos \frac{\phi}{2} dc + \omega r (\sqrt{2} - 1) \int_C^E C \cos \frac{\phi}{2} dc$$

$$+ \sqrt{2} \omega r \int_C^E C \sin \frac{\phi}{2} dc - \frac{P_0 r}{\sqrt{2}} \int_C^E \sin \frac{\phi}{2} dc = 0$$

or

$$X = - \frac{\omega'}{2} \frac{\int_A^B x^2 dc}{\int_A^E dc} - P_0 \frac{\int_B^E x dc}{\int_A^E dc} + \frac{P_0 a}{2} \frac{\int_B^E dc}{\int_A^E dc}$$

$$+ \omega \frac{\int_A^E C x dc}{\int_A^E dc} - \omega r \frac{\int_A^C C \sin \frac{\phi}{2} dc}{\int_A^E dc} - P_0 r \left(1 - \frac{1}{\sqrt{2}} \right) \frac{\int_C^E \cos \frac{\phi}{2} dc}{\int_A^E dc}$$

$$- \omega r (\sqrt{2} - 1) \frac{\int_C^E C \cos \frac{\phi}{2} dc}{\int_A^E dc} - \sqrt{2} \omega r \frac{\int_C^E C \sin \frac{\phi}{2} dc}{\int_A^E dc}$$

$$+ \frac{P_{\phi} r}{\sqrt{2}} \frac{\int_A^E \sin \frac{\phi}{2} dc}{\int_A^E dc}$$

But, referring to the figure (2), we have

$$x = r \sin \phi$$

$$a = r \sin \alpha$$

$$C = r \phi$$

$$dc = r d\phi$$

where ϕ denotes the inclination of the tangent at any point (x, y) to the horizontal.

Therefore, we can find, by carrying out the integrations as before;

$$X(\text{or } M_A) = -\frac{P_{\phi} r}{2\pi \sin \alpha} \left\{ -\frac{\sin 2\phi}{4} + \frac{\phi}{2} \right\}_0^{\alpha} + \frac{P_{\phi} r (\pi - \alpha) \sin \alpha}{2\pi}$$

$$- \frac{P_{\phi} r}{\pi} (-\cos \phi)_0^{\pi} + \frac{P_{\phi} r}{\pi} - \frac{8P_{\phi} r}{\pi^2} (\sqrt{2} - 1)$$
