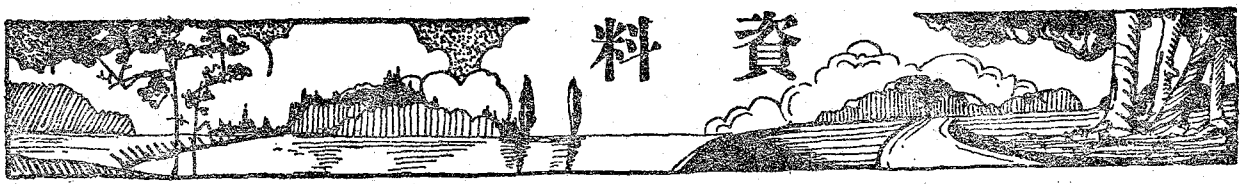

曲げモーメントを受ける單鐵筋丁形梁の應力度算定係數表(下)

小野竹之助

§3 曲げ應力度の算定係數表

§2に於て求めた(1')式乃至(5')式に於て、$n=10$ とし、

p 及びt/dの夫々の値に對する k, j, x_c, x_s 及び m の數値を表示すれば、次表の如くなる。

茲に

表—1 は $t/d=0.10$ 及び 0.12

表—1

p	$t/d=0.10$					$t/d=0.12$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.10	0.136	0.960	16.45	1042.0	63.3	0.132	0.957	15.94	1045.3	65.6
0.15	0.174	0.957	14.67	696.8	47.5	0.164	0.952	13.79	700.6	50.8
0.20	0.208	0.955	13.77	523.4	38.0	0.194	0.949	12.71	526.9	41.5
0.25	0.240	0.954	13.24	419.1	31.7	0.222	0.947	12.05	422.2	35.0
0.30	0.269	0.954	12.88	349.5	27.1	0.248	0.946	11.62	352.2	30.3
0.35	0.296	0.953	12.62	299.7	23.7	0.272	0.946	11.30	302.1	26.7
0.40	0.321	0.953	12.43	262.3	21.1	0.295	0.945	11.07	264.5	23.9
0.45	0.345	0.953	12.28	233.2	19.0	0.316	0.954	10.89	235.2	21.6
0.50	0.367	0.953	12.16	209.9	17.3	0.336	0.944	10.74	211.8	19.7
0.55	0.387	0.952	12.06	190.9	15.8	0.355	0.944	10.62	192.6	18.1
0.60	0.406	0.952	11.97	175.0	14.6	0.373	0.944	10.52	176.6	16.8
0.65	0.424	0.952	11.90	161.6	13.6	0.390	0.944	10.44	163.0	15 6
0.70	0.441	0.952	11.85	150.0	12.7	0.406	0.943	10.36	151.4	14.6
0.75	0.457	0.952	11.79	140.0	11.9	0.422	0.943	10.30	141.3	13.7
0.80	0.472	0.952	11.75	131.3	11.2	0.436	0.943	10.25	132.5	12.9
0.85	0.486	0.952	11.71	123.6	10.6	0.450	0.943	10.20	124.7	12.2
0.90	0.500	0.952	11.67	116.7	10.0	0.463	0.943	10.15	117.8	11.6
0.95	0.513	0.952	11.64	110.6	9.5	0.475	0.943	10.11	111.6	11.0
1.00	0.525	0.952	11.61	105.1	9.0	0.487	0.943	10.08	106.1	10.5
1.10	0.548	0.952	11.56	95.5	8.3	0.510	0.943	10.02	96.4	9.6
1.20	0.568	0.952	11.52	87.6	7.6	0.530	0.943	9.97	88.4	8.9
1.30	0.587	0.951	11.49	80.8	7.0	0.549	0.942	9.93	81.6	8.2
1.40	0.604	0.951	11.46	75.1	6.6	0.566	0.942	9.89	75.8	7.7
1.50	0.620	0.951	11.43	70.1	6.1	0.582	0.942	9.86	70.7	7.2

表—2

p	$t/d=0.14$					$t/d=0.15$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.15	0.160	0.948	13.39	703.1	52.5	0.159	0.947	13.32	703.8	52.8
0.20	0.186	0.944	12.12	529.6	43.7	0.184	0.942	11.95	530.6	44.4
0.25	0.211	0.942	11.35	424.8	37.4	0.207	0.939	11.13	425.9	38.3
0.30	0.234	0.940	10.84	354.6	32.7	0.229	0.937	10.57	355.7	33.6
0.35	0.256	0.939	10.47	304.3	29.1	0.250	0.936	10.18	305.3	30.0
0.40	0.277	0.938	10.20	266.5	26.1	0.270	0.935	9.88	267.5	27.1
0.45	0.296	0.937	9.98	237.1	23.8	0.288	0.934	6.65	238.0	24.7
0.50	0.315	0.937	9.81	213.5	21.8	0.306	0.933	9.46	214.3	22.7
0.55	0.332	0.936	9.67	194.2	20.1	0.323	0.933	9.31	195.0	20.9
0.60	0.349	0.936	9.55	178.1	18.6	0.339	0.932	9.18	178.8	19.5
0.65	0.365	0.936	9.45	164.4	17.4	0.355	0.932	9.07	165.1	18.2
0.70	0.380	0.935	9.36	152.7	16.3	0.369	0.931	8.98	153.4	17.1
0.75	0.394	0.935	9.29	142.6	15.4	0.383	0.931	8.90	143.2	16.1
0.80	0.408	0.935	9.22	133.7	14.5	0.397	0.931	8.83	134.3	15.2
0.85	0.421	0.935	9.16	125.9	13.7	0.410	0.931	8.88	126.4	14.4
0.90	0.434	0.934	9.11	118.9	13.0	0.422	0.930	8.71	119.4	13.7
0.95	0.446	0.934	9.07	112.7	12.4	0.434	0.930	8.67	113.2	13.1
1.00	0.458	0.934	9.03	107.0	11.9	0.445	0.930	8.62	107.5	12.5
1.10	0.479	0.934	8.96	97.3	10.9	0.466	0.930	8.54	97.8	11.4
1.20	0.499	0.934	8.90	89.2	10.0	0.486	0.930	8.48	89.6	10.6
1.30	0.518	0.934	8.85	82.4	9.3	0.504	0.929	8.43	82.8	9.8
1.40	0.535	0.934	8.80	76.5	8.7	0.522	0.929	8.38	76.9	9.2
1.50	0.551	0.933	8.77	71.4	8.1	0.538	0.929	8.34	71.8	8.6

表—3

p	$t/d=0.16$					$t/d=0.18$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.20	0.182	0.941	11.84	531.4	44.9	0.181	0.940	11.76	532.1	45.2
0.25	0.204	0.937	10.96	426.8	38.9	0.201	0.934	10.77	428.1	39.7
0.30	0.225	0.935	10.37	356.6	34.4	0.220	0.931	10.10	358.1	35.5
0.35	0.245	0.933	9.95	306.3	30.8	0.238	0.928	9.62	307.8	32.0
0.40	0.264	0.932	9.63	268.4	27.9	0.255	0.926	9.26	269.9	29.1
0.45	0.282	0.931	9.38	238.8	25.5	0.272	0.925	8.98	240.3	26.8
0.50	0.299	0.930	9.18	215.1	23.4	0.288	0.924	8.75	216.5	24.7
0.55	0.315	0.929	9.01	195.7	21.7	0.303	0.923	8.57	197.1	23.0
0.60	0.331	0.929	8.88	179.5	20.2	0.318	0.922	8.41	180.8	21.5
0.65	0.346	0.928	8.76	165.8	18.9	0.331	0.921	8.28	167.0	20.2
0.70	0.360	0.928	8.66	154.0	17.8	0.345	0.921	8.17	155.2	19.0
0.75	0.374	0.927	8.58	143.8	16.8	0.358	0.920	8.07	144.9	18.0
0.80	0.387	0.927	8.50	134.9	15.9	0.370	0.920	7.98	135.9	17.0
0.85	0.399	0.927	8.43	127.0	15.0	0.382	0.919	7.91	128.0	16.2
0.90	0.411	0.926	8.38	119.9	14.3	0.393	0.919	7.84	120.9	15.4
0.95	0.423	0.926	8.32	113.6	13.7	0.404	0.919	7.78	114.6	14.7
1.00	0.434	0.926	8.28	108.0	13.1	0.415	0.918	7.72	108.9	14.1
1.10	0.455	0.926	8.19	98.2	12.0	0.435	0.918	7.63	99.0	13.0
1.20	0.474	0.925	8.12	90.1	11.1	0.454	0.918	7.55	90.8	12.0
1.30	0.492	0.925	8.07	83.1	10.3	0.472	0.917	7.49	83.9	11.2
1.40	0.509	0.925	8.02	77.2	9.6	0.488	0.917	7.43	77.9	10.5
1.50	0.525	0.925	7.97	72.1	9.0	0.504	0.917	7.38	72.7	9.9

表—4

	p	$t/d=0.20$					$t/d=0.22$				
資	%	k	j	x_c	x_a	m	k	j	x_c	x_a	m
	0.25	0.200	0.933	10.71	428.6	40.0					
料	0.30	0.217	0.928	9.97	359.0	36.0					
	0.35	0.234	0.925	9.44	308.9	32.7	0.232	0.923	9.36	309.6	33.1
	0.40	0.250	0.922	9.04	271.1	30.0	0.247	0.919	8.92	271.9	30.5
	0.45	0.265	0.920	8.72	241.5	27.7	0.261	0.917	8.57	242.4	28.3
	0.50	0.280	0.919	8.47	217.7	25.7	0.275	0.914	8.29	218.7	26.4
	0.55	0.294	0.917	8.26	198.2	24.0	0.288	0.913	8.06	199.2	24.7
	0.60	0.308	0.916	8.09	181.9	22.5	0.301	0.911	7.87	182.9	23.3
	0.65	0.321	0.915	7.94	168.1	21.2	0.313	0.910	7.70	169.1	22.0
	0.70	0.333	0.914	7.81	156.2	20.0	0.325	0.909	7.56	157.2	20.8
	0.75	0.345	0.914	7.70	145.9	18.9	0.336	0.908	7.44	146.9	19.7
	0.80	0.357	0.913	7.61	136.9	18.0	0.347	0.907	7.33	137.8	18.8
	0.85	0.368	0.913	7.52	128.9	17.1	0.358	0.906	7.24	129.8	17.9
	0.90	0.379	0.912	7.45	121.8	16.4	0.368	0.906	7.16	122.7	17.1
	0.95	0.390	0.912	7.38	115.5	15.7	0.378	0.905	7.08	116.3	16.4
	1.00	0.400	0.911	7.32	109.8	15.0	0.388	0.905	7.01	110.6	15.8
	1.10	0.419	0.910	7.21	99.9	13.8	0.407	0.904	6.90	100.6	14.6
三一	1.20	0.438	0.910	7.12	91.6	12.9	0.424	0.903	6.80	92.3	13.6
	1.30	0.455	0.909	7.05	84.6	12.0	0.441	0.902	6.71	85.3	12.7
	1.40	0.471	0.909	6.98	78.6	11.2	0.456	0.902	6.64	79.2	11.9
	1.50	0.486	0.909	6.93	73.4	10.6	0.471	0.901	6.58	74.0	11.2

表—5

p	$t/d=0.24$					$t/d=0.25$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.40	0.246	0.918	8.87	272.3	30.7					
0.45	0.259	0.915	8.49	243.0	28.6	0.258	0.914	8.47	243.1	28.7
0.50	0.272	0.912	8.18	219.4	26.8	0.271	0.911	8.16	219.6	26.9
0.55	0.284	0.909	7.93	200.0	25.2	0.283	0.908	7.90	200.2	25.4
0.60	0.296	0.907	7.72	183.7	23.8	0.294	0.906	7.68	184.0	24.0
0.65	0.308	0.906	7.54	169.9	22.5	0.306	0.904	7.49	170.2	22.7
0.70	0.319	0.904	7.39	158.0	21.4	0.316	0.902	7.33	158.3	21.6
0.75	0.330	0.903	7.26	147.7	20.4	0.327	0.901	7.19	148.0	20.6
0.80	0.340	0.902	7.14	138.6	19.4	0.337	0.900	7.07	139.0	19.7
0.85	0.350	0.901	7.04	130.6	18.6	0.347	0.898	6.96	130.9	18.8
0.90	0.360	0.900	6.94	123.5	17.8	0.357	0.897	6.86	123.8	18.0
0.95	0.370	0.899	6.86	117.1	17.1	0.366	0.897	6.78	117.4	17.3
1.00	0.379	0.899	6.79	111.3	16.4	0.375	0.896	6.70	111.6	16.7
1.10	0.397	0.897	6.66	101.3	15.2	0.392	0.894	6.56	101.6	15.5
1.20	0.413	0.896	6.55	93.0	14.2	0.409	0.893	6.45	93.3	14.5
1.30	0.429	0.896	6.46	85.9	13.3	0.424	0.892	6.35	86.2	13.6
1.40	0.444	0.895	6.38	79.8	12.5	0.439	0.892	6.27	80.1	12.8
1.50	0.458	0.894	6.31	74.6	11.8	0.453	0.891	6.20	74.8	12.1

表—6

p	$t/d=0.26$					$t/d=0.28$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.50	0.270	0.910	8.14	219.7	27.0					
0.55	0.282	0.907	7.87	200.4	25.5	0.281	0.906	7.85	200.6	23.6
0.60	0.293	0.905	7.64	184.2	24.1	0.292	0.903	7.60	184.6	24.3
0.65	0.304	0.902	7.45	170.5	22.9	0.302	0.900	7.39	170.9	23.1
0.70	0.315	0.901	7.28	158.6	21.8	0.312	0.898	7.21	159.1	22.1
0.75	0.325	0.899	7.13	148.3	20.8	0.322	0.896	7.06	148.8	21.1
0.80	0.335	0.898	7.01	139.3	19.9	0.331	0.894	6.92	139.8	20.2
0.85	0.344	0.896	6.89	131.3	19.0	0.340	0.893	6.80	131.8	19.4
0.90	0.354	0.895	6.79	124.1	18.3	0.349	0.891	6.69	124.7	18.6
0.95	0.363	0.894	6.70	117.7	17.6	0.358	0.890	6.59	118.3	17.9
1.00	0.372	0.893	6.62	111.9	16.9	0.366	0.889	6.50	112.5	17.3
1.10	0.389	0.892	6.48	101.9	15.7	0.383	0.887	6.35	102.5	16.1
1.20	0.405	0.891	6.36	93.6	14.7	0.398	0.885	6.22	94.1	15.1
1.30	0.420	0.889	6.26	86.5	13.8	0.413	0.884	6.11	87.0	14.2
1.40	0.434	0.888	6.18	80.4	13.0	0.427	0.883	6.02	80.9	13.4
1.50	0.448	0.888	6.10	75.1	12.3	0.440	0.882	5.94	75.6	12.7

表—7

p	$t/d=0.30$					$t/d=0.32$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.65	0.301	0.900	7.38	171.0	23.2					
0.70	0.311	0.897	7.19	159.3	22.2					
0.75	0.320	0.894	7.02	149.1	21.2					
0.80	0.329	0.892	6.87	140.1	20.4	0.328	0.891	6.85	140.3	20.5
0.85	0.338	0.890	6.74	132.2	19.6	0.336	0.888	6.71	132.4	19.7
0.90	0.346	0.888	6.62	125.1	18.9	0.344	0.836	6.59	125.4	19.0
0.95	0.354	0.887	6.52	118.7	18.2	0.352	0.884	6.47	119.0	184
1.00	0.362	0.885	6.42	113.0	17.6	0.360	0.883	6.37	113.3	17.8
1.10	0.378	0.883	6.26	103.0	16.5	0.375	0.880	6.20	103.3	16.7
1.20	0.393	0.881	6.12	94.6	15.5	0.389	0.877	6.05	95.0	15.7
1.30	0.407	0.879	6.00	87.5	14.6	0.403	0.875	5.93	87.9	14.8
1.40	0.420	0.878	5.90	81.4	13.8	0.416	0.873	5.82	81.8	14.1
1.50	0.433	0.876	5.82	76.1	13.1	0.428	0.872	5.72	76.5	13.4

表—8

p	$t/d=0.34$					$t/d=0.35$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
0.90	0.344	0.885	6.57	125.5	19.1					
0.95	0.351	0.883	6.45	119.2	18.5	0.351	0.883	6.45	119.2	18.5
1.00	0.359	0.881	6.35	113.5	17.9	0.358	0.881	6.34	113.5	17.9
1.10	0.373	0.877	6.16	103.6	16.8	0.372	0.877	6.15	103.7	16.9
1.20	0.387	0.874	6.00	95.3	15.9	0.386	0.873	5.99	65.4	15.9
1.30	0.400	0.872	5.87	88.2	15.0	0.398	0.871	5.85	88.3	15.1
1.40	0.412	0.870	5.76	82.1	14.3	0.411	0.868	5.73	82.3	14.3
1.50	0.424	0.868	5.66	76.8	13.6	0.422	0.866	5.63	77.0	13.7

表—9

p	$t/d=0.36$					$t/d=0.38$				
%	k	j	x_c	x_s	m	k	j	x_c	x_s	m
1.10	0.372	0.876	6.14	103.7	16.9					
1.20	0.385	0.873	5.98	95.5	16.0	0.384	0.872	5.97	95.6	16.0
1.30	0.398	0.870	5.84	88.5	15.2	0.396	0.868	5.82	88.6	15.2
1.40	0.410	0.867	5.72	82.4	14.4	0.408	0.865	5.69	82.6	14.5
1.50	0.421	0.865	5.61	77.1	13.7	0.419	0.862	5.58	77.3	13.9

表—10

p	$t/d=0.40$				
%	k	j	x_c	x_s	m
1.40	0.407	0.867	5.68	82.6	14.5
1.50	0.418	0.861	5.56	77.4	13.9